VVATERS THE SCIENCE OF WHAT'S POSSIBLE.

# Techniques for Improving the Efficiency of Large Volume Loading in Preparative Liquid Chromatography

Jo-Ann M. Jablonski, Andrew J. Aubin, and Wendy Harrop Waters Corporation, Milford, MA, USA

# **APPLICATION BENEFITS**

- Large volume sample loading reduces the number of runs, time, and solvent required for the isolation of compounds from weak diluents, thereby improving the efficiency of the purification process.
- Large volumes of sample with low concentration in weak solvent can be isolated more quickly by increasing loading with simple HPLC method and plumbing changes.
- Mass-directed purification clearly identifies the product of interest and makes isolation easy.

#### WATERS SOLUTIONS

AutoPurification™ System ACQUITY® QDa® Detector OBD™ Prep Columns At-Column Dilution

#### **KEY WORDS**

Prep chromatography, large volume sample loading, impurity isolation, mass-directed purification, pump loading, autopurification, ACQUITY QDa Detector, OBD Prep columns, At-Column Dilution

# INTRODUCTION

Preparative scale liquid chromatography can be challenging to the purification scientist in many ways, but effective sample loading directly influences the success of compound isolation. While the objectives of prep chromatography include achieving high mass load on the column and employing rugged generic chromatography, two conflicting principles almost always play a role in the approach used to realize these objectives. First, strong solvents dissolve samples but distort chromatographic peaks due to the inability of the sample to properly interact with the column packing. Second, weak solvents as sample diluents give good chromatography but do not dissolve samples at high concentration. Low sample concentration ultimately results in large injection volumes which are difficult to handle and generally result in poor chromatography. Although these challenges are well-known among chromatographers, with easy modifications to the HPLC system plumbing and with mass detection, these issues can be addressed satisfactorily using at-column dilution.<sup>1</sup> In this study, we illustrate and compare different techniques for improving the efficiency of loading large volumes of dilute sample in weak solvent for compound isolation. The impact of each technique on the overall purification efficiency is discussed.

# [APPLICATION NOTE]

# EXPERIMENTAL

### Conditions

Analytical column						
and flow rate:	XBridge <sup>®</sup> BEH Shield RP18,					
	$4.6x50$ mm, 5 $\mu\text{m};1.46$ mL/min					
Prep column						
and flow rate:	XBridge BEH Shield RP18 OBD Prep,					
	19 x 50 mm, 5 μm; 25 mL/min					
Mobile phase A:	0.1% formic acid in water					
Mobile phase B:	0.1% formic acid in acetonitrile					
Makeup solvent:	50:50 water:acetonitrile,					
	0.01% formic acid					
Cone voltage:	15 V					
Probe temp.:	500 °C					
lonization mode:	ES+, continuum					
Sampling frequency:	5 Hz					
Scan range:	100–650 amu					
Wavelength:	274 nm					
Gradients and						
injection volumes:	as noted in figures					
Sample:	10 bags Lipton Green Tea extracted with					
	1L hot water for 10 minutes and filtered					

#### Instrumentation

Waters AutoPurification System: 2545 Binary Gradient Module, 2767 Sample Manager, System Fluidics Organizer, 8–30 mL Flow Splitter, two 515 HPLC pumps, 2998 Photodiode Array Detector, ACQUITY QDa Detector



# DISCUSSION

Epigallocatechin gallate (EGCG) and epicatechin gallate (ECG), two of the many catechins found in green tea, were chosen as the compounds of interest for illustrating the concepts in these experiments. A loading study was performed to determine the amount of crude green tea extract that could be loaded on the analytical column, yet still give good resolution for the EGCG and ECG. The 200  $\mu$ L maximum volume showed good resolution at 274 nm, but with mass detection, the two peaks of interest were clearly identified (Figure 1) even when running a fast screening gradient.

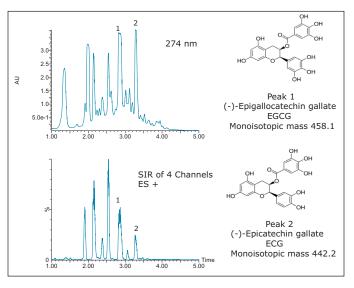


Figure 1. 200  $\mu L$  crude green tea extract injected on the 4.6 x 50 mm column. Gradient: 5–50% B in 5 min.

Peak 1 = Epigallocatechin gallate, M + H 459.1; Peak 2 = Epicatechin gallate, M + H 443.2 Geometric scaling from 200  $\mu$ L on the analytical column to 3412  $\mu$ L on the 19 x 50 mm preparative column gave acceptable chromatography with easy mass-directed fraction collection, as did doubling the injection volume to 6824  $\mu$ L (Figure 2). Fraction analysis (not shown) at 274 nm for EGCG and ECG, however, indicated purities of approximately 94% for both EGCG preps, and 40% for the 3.4 mL and 72% for the 6.8 mL ECG preps.

Focusing the gradient<sup>2</sup> and isolating the two catechins from a 6824  $\mu$ L injection of the crude extract improved the fraction purities of both the main product (EGCG) and the impurity (ECG) to 100% and 80%, respectively (Figure 3).

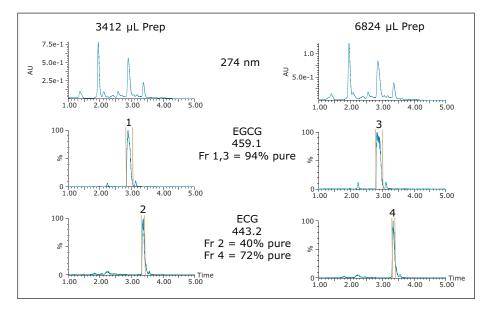


Figure 2. 3.4 and 6.8 mL injections of crude green tea extract on the 19 x 50 mm column. Mass chromatograms are SIR channels. Gradient: 5–50% B in 5 min.

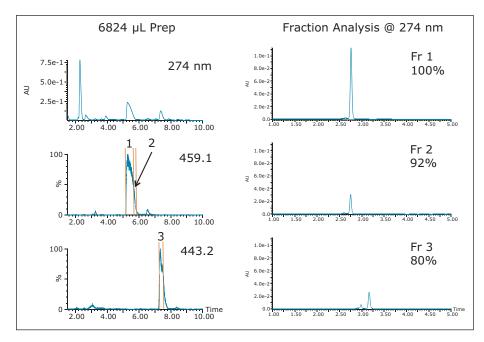


Figure 3. 6.8 mL injection of crude green tea extract on the 19 x 50 mm column. Mass chromatograms are SIR channels. Prep gradient: 10-30% B in 11 min. Analysis gradient: 5-50% B in 5 min, 20  $\mu$ L.

# [APPLICATION NOTE]

Large volumes of sample in weak solvent necessitate loading as much sample as possible to improve purification efficiency while maintaining enough resolution to successfully isolate the compounds of interest. Since the purity of the desired product was excellent with a 6.8 mL injection, and the resolution between the EGCG and its closely-eluting neighbors was also acceptable, a 21 mL injection was performed. Despite the three-fold increase in sample size, the fraction analysis showed comparable purity to the 6.8 mL injection (Figure 4).

Loading large sample volumes onto the prep column would be more efficient if a pump was used. With a successful 21 mL prep already performed using a syringe for sample introduction, the same volume was loaded in a second prep using a pump to load the sample. The plumbing configuration was analogous to the setup used for at-column dilution, a technique described in detail in previous communications. The sample extract was pumped to one side of a tee at 7 mL/min where it was mixed with the system mobile phase at 100% A (water, 0.1% formic acid) flowing at 18 mL/min (total flow rate 25 mL/min) and subsequently deposited onto the head of the column (Figure 5). After the sample loading line was chased with water, the gradient was started. The chromatography for the sample loaded with the pump was identical to the chromatography for the sample injected by syringe (Figure 6). Fraction analysis results were also the same.

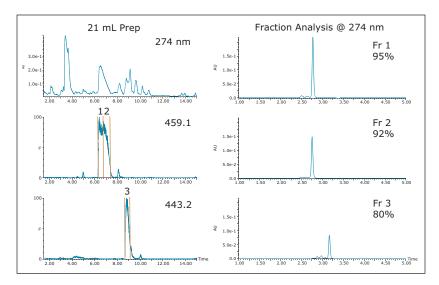


Figure 4. 21 mL injection of crude green tea extract on the 19 x 50 mm column using a 30 mL loop. Mass chromatograms are SIR channels. Prep gradient: 10–30% B in 11 min. Analysis gradient: 5–50% B in 5 min, 20 μL.

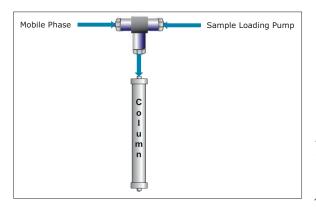


Figure 5. Diagram for using a loading pump to introduce large sample volumes onto a column for compound isolation.

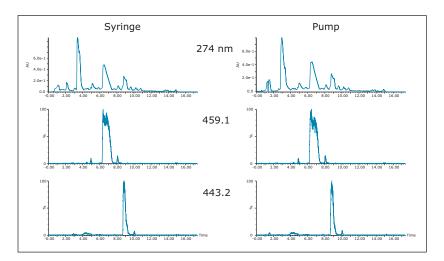


Figure 6. Comparison of two 21 mL prep isolations with different modes of sample loading.

With a 21 mL sample loading successfully performed, and with 1 liter of extract to process, loading even larger sample volumes would clearly increase the efficiency of the product and impurity isolation. Table 1 shows the benefit of increasing sample loading volumes with the reduction in the number of chromatographic runs, decreased solvent usage and time savings. Consequently, the loading pump was used to introduce 40 and 100 mL sample extract volumes onto the 19 x 50 mm column for isolation (Figures 7, 9). These sample extracts were pumped onto the column at 10 mL/min, mixing with the chromatographic pump flow at 15 mL/min, for a total flow rate of 25 mL/min. The total flow rate was maintained at the flow rate used to time the system for fraction collection, ensuring consistent collection performance. The 100 mL isolation showed an earlier target compound elution time due to the extremely high sample load and a modification of the gradient method. Despite the large volume which was loaded, mass-directed purification unambiguously identified the peaks of interest. While the 21 and 40 mL samples were loaded with a pump and the lines chased with water, the plumbing after sample loading was returned to the typical conventional configuration without the tee for sample addition. To make the process less cumbersome, for the 100 mL extract isolation, the sample loading pump plumbing was preserved throughout the gradient method. Once the aqueous green tea extract was loaded, water was added to the sample loading vessel and introduced as part of the weak solvent composition throughout the gradient.

The gradient method was modified to account for the aqueous contribution from the loading pump (Figure 8).

Loading Volume vs. Effect on Efficiency										
Loading			Chromato	graphy	Usage					
Vol	Mode	Time	No. Runs	Time	Solvent	Time				
(mL)	Mode	(min)	NO. RUIIS	(min)	(L)	(hr)				
6.8	Loop	2	147	16.4	68	45				
21	Loop	3	47	17.4	24	16				
40	Pump	4	25	17.4	13	9				
100	Pump	10	10	17.4	7	5				

Table 1. Loading volume's effect on the calculated processing efficiency of 1 liter of crude extract.

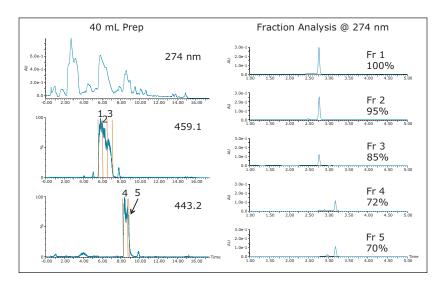


Figure 7. 40 mL green tea extract on the 19 x 50 mm column. Mass chromatograms are SIR channels. Prep gradient: 10-30% B in 11 min. Analysis gradient: 5-50% B in 5 min, 20  $\mu$ L.

Gradient Method Conventional Plumbing			Gradient Method Sample Loading Pump Plumbing					
Time	Flow	%A	%B		Time	Flow	%A	%В
0.00	25	95	5	-	0.00	24	91	9
2.00	25	90	10		2.00	24	86	14
13.17	25	70	30		13.17	24	66	34
13.27	25	5	95		13.27	24	1	99
14.27	25	5	95		14.27	24	1	99
14.37	25	95	5		14.37	24	91	9
17.40	25	95	5		17.40	24	91	9
				Sample volume = 100 mL Sample loading flow rate = 10 mL/min Loading pump flow rate during gradient = 1.0 mL/min water 1.0 mL/min = 4% of the total flow Total gradient method flow rate = 25 mL/min				

Figure 8. Gradient method comparison for conventional plumbing and sample loading pump plumbing configurations. The sample loading pump gradient method was modified to account for the loading pump's contribution to the total flow rate and solvent composition.

Fraction analysis results for the 100 mL isolation were comparable to the purities obtained from the 21 mL and 40 mL sample loading experiments with two very pure EGCG (459.1) fractions and similar purities for ECG (443.2) (Figure 10).

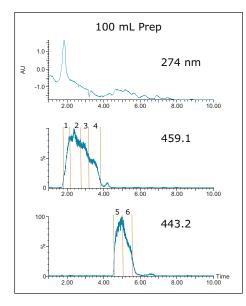


Figure 9. 100 mL green tea extract on the 19 x 50 mm column. Mass chromatograms are SIR channels. Prep gradient: 10–30% B in 11 min, sample loading pump plumbing configuration.

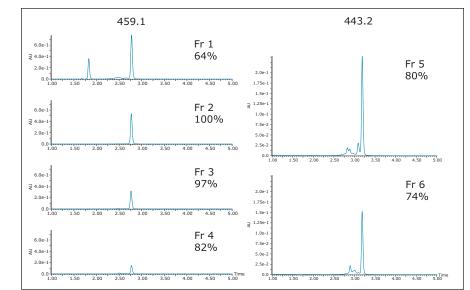


Figure 10. Fraction analysis from the 100 mL isolation. Analysis gradient: 5–50% B in 5 min, 20  $\mu$ L.

6

#### CONCLUSIONS

In this study, isolation of compounds of low concentration from large volumes of weak solvent was effectively accomplished with simple HPLC method and plumbing modifications. Focusing the gradient improved the quality of the target compound isolation by increasing the resolution between contaminant peaks and permitting increased loading on the column. Whether using a larger loop and syringe or adding a tee and a loading pump to the HPLC configuration for sample introduction, the chromatography was remarkably consistent and isolated products had comparable purities.

Detection plays an important role in the success of product isolation. While large sample volumes very rapidly distort UV chromatograms and make product peak identification ambiguous, mass-directed purification clearly reveals where the target compound elutes and makes fraction collection easier. As the amount of sample volume increases, the efficiency of the overall compound isolation improves by reducing the solvent usage and time for completing the purification process.

#### References

- 1. Wheat T, et.al. At-Column Dilution. Waters Application Note 71500078010rA. 2003.
- Jablonski J, Wheat T, Diehl D. Developing Focused Gradients for Isolation and Purification. Waters Technical Note <u>720002955EN</u>. September 2009.



Waters, The Science of What's Possible, ACQUITY, QDa and XBridge are registered trademarks of Waters Corporation. AutoPurification and OBD are trademarks of Waters Corporation. All other trademarks are the property of their respective owners. Waters Corporation 34 Maple Street Milford, MA 01757 U.S.A. T: 1 508 478 2000 F: 1 508 872 1990 www.waters.com